

ENEE 381 Problem Set #7, 2002. SOLUTIONS

(1) $a := 15 \cdot 10^{-3}$ conductor spacing
 $c_0 := 2.998 \cdot 10^8$ velocity of light in a vacuum

The formula for the cutoff frequency is

$$v_c = \frac{m \cdot c}{2 \cdot a} \quad c \text{ is velocity of light in material between planes}$$

The TE_m and TM_m have the same cutoff frequency, which is determined by the integer m
 In air, for $m=1$

$$v_c := \frac{c_0}{2 \cdot a}$$

$$v_c = 9.993 \times 10^9 \quad 10\text{GHz}$$

For $m=2$

$$v_c := \frac{2 \cdot c_0}{2 \cdot a}$$

$$v_c = 1.999 \times 10^{10} \quad 20\text{GHz}$$

For $m=3$

$$v_c := \frac{3 \cdot c_0}{2 \cdot a}$$

$$v_c = 2.998 \times 10^{10} \quad 30\text{GHz}$$

With $\epsilon_r=4$ $c := \frac{c_0}{2}$

so corresponding cutoff frequencies are 5GHz, 10GHz, and 15GHz

With an air-filled line and 8GHz excitation, all modes are cutoff. In this case the attenuation constant α is

$$i := 1, 2, \dots, 3 \quad v := 8 \cdot 10^9 \quad v_{c_1} := 10 \cdot 10^9 \quad v_{c_2} := 20 \cdot 10^9 \quad v_{c_3} := 30 \cdot 10^9$$

$$\alpha_i := i \cdot \frac{\pi}{a} \cdot \sqrt{1 - \left(\frac{v}{v_{c_i}} \right)^2}$$

$$\frac{1}{\alpha_1} = 7.958 \times 10^{-3}$$

$$\frac{1}{\alpha_2} = 2.605 \times 10^{-3}$$

$$\frac{1}{\alpha_3} = 1.651 \times 10^{-3}$$

(2) The formula for the cutoff frequency is for a mode $TE_{m,n}$ or $TM_{m,n}$ is

$$v_{c_{m,n}} = \frac{c}{2 \cdot \pi} \cdot \sqrt{\left(\frac{m \cdot \pi}{a}\right)^2 + \left(\frac{n \cdot \pi}{b}\right)^2} \quad a := 30 \cdot 10^{-3} \quad b := 15 \cdot 10^{-3}$$

$$v := 10 \cdot 10^9$$

For an air-filled guide $c := c_0$

$m := 1, 2 \dots 3$ $n := 0, 1 \dots 2$ different mode subscripts

$$v_{c_{m,n}} := \frac{c}{2 \cdot \pi} \cdot \sqrt{\left(\frac{m \cdot \pi}{a}\right)^2 + \left(\frac{n \cdot \pi}{b}\right)^2}$$

$$v_{c_{1,0}} = 4.997 \times 10^9 \quad v_{c_{1,1}} = 1.117 \times 10^{10} \quad v_{c_{1,2}} = 2.06 \times 10^{10}$$

$$v_{c_{2,1}} = 1.413 \times 10^{10} \quad v_{c_{2,2}} = 2.235 \times 10^{10} \quad v_{c_{2,0}} = 9.993 \times 10^9$$

The attenuation constant is

$$\alpha_{m,n} := \sqrt{\left(\frac{m \cdot \pi}{a}\right)^2 + \left(\frac{n \cdot \pi}{b}\right)^2} \cdot \sqrt{1 - \left(\frac{v}{v_{c_{m,n}}}\right)^2}$$

No attenuation for TE_{10} mode and TE_{20} mode. For other modes

$$\frac{1}{\alpha_{1,1}} = 9.575 \times 10^{-3} \quad \frac{1}{\alpha_{2,2}} = 2.388 \times 10^{-3}$$

$$\frac{1}{\alpha_{1,2}} = 2.649 \times 10^{-3} \quad \frac{1}{\alpha_{2,1}} = 4.778 \times 10^{-3}$$

With a dielectric $c := \frac{c_0}{2}$

$$v_{c_{m,n}} := \frac{c}{2 \cdot \pi} \cdot \sqrt{\left(\frac{m \cdot \pi}{a}\right)^2 + \left(\frac{n \cdot \pi}{b}\right)^2}$$

$$v_{c_{1,0}} = 2.498 \times 10^9 \quad v_{c_{1,1}} = 5.586 \times 10^9 \quad v_{c_{1,2}} = 1.03 \times 10^{10}$$

$$v_{c_{2,1}} = 7.066 \times 10^9 \quad v_{c_{2,2}} = 1.117 \times 10^{10} \quad v_{c_{2,0}} = 4.997 \times 10^9$$

The attenuation constant is

$$\alpha_{m,n} := \sqrt{\left(\frac{m \cdot \pi}{a}\right)^2 + \left(\frac{n \cdot \pi}{b}\right)^2} \cdot \sqrt{1 - \left(\frac{v}{v_{c_{m,n}}}\right)^2}$$

No attenuation for TE₁₀, TE₂₀, TE₁₁ and TM₁₁ modes. For other modes

$$\frac{1}{\alpha_{1,2}} = 9.653 \times 10^{-3} \quad \frac{1}{\alpha_{2,2}} = 4.787 \times 10^{-3}$$

(3) $n := 1.5$ $\theta_1 := 80 \cdot \text{deg}$ Take $\lambda = 1 \mu\text{m}$ $\lambda := 10^{-6}$

$$\theta_2 := \text{asin}(n \cdot \sin(\theta_1))$$

$$\theta_2 = 1.571 - 0.942i \quad \text{Note that because of total internal reflection } \theta_2 \text{ is complex}$$

$$\cos(\theta_2) = 1.087i$$

Take the wave to be a P-wave

$$\rho := \frac{n \cdot \cos(\theta_2) - \cos(\theta_1)}{n \cdot \cos(\theta_2) + \cos(\theta_1)}$$

$$(|\rho|)^2 = 1 \quad \text{all energy reflects}$$

The propagation constant of the wave in the z-direction (perpendicular to the boundary) on the air side of the boundary is with

$$k_{\text{air}} := 2 \cdot \frac{\pi}{\lambda}$$

$$k_z := k_{\text{air}} \cdot \cos(\theta_2)$$

$$k_z = 6.832i \times 10^6 \quad \text{Note that this is imaginary}$$

$$\alpha := \text{Im}(k_z)$$

$$\alpha = 6.832 \times 10^6$$

$$\frac{1}{\alpha} = 1.464 \times 10^{-7}$$

$$\frac{1}{\alpha \cdot \lambda} = 0.146 \quad \text{penetrates about 0.146 wavelengths}$$

(4) For the TE₁₀ mode the cutoff frequency is $v_c = \frac{c}{2 \cdot a}$

$v := 10 \cdot 10^9$ input frequency $c := 2.998 \cdot 10^8$ velocity of light

In air $v_c := \frac{c}{2 \cdot a}$ $a := 50 \cdot 10^{-3}$ $b := 10 \cdot 10^{-3}$ guide dimensions

$v_c = 2.998 \times 10^9$ Note that $\frac{c}{2 \cdot b} = 1.499 \times 10^{10}$ so mode only propagates in one orientation

In dielectric-filled section $c := \frac{c_0}{2}$ $\lambda_0 := \frac{c_0}{v}$ wavelength in air

$v d_c := \frac{c}{2 \cdot a}$ new cutoff frequency

$v d_c = 1.499 \times 10^9$ $\lambda_d := \frac{c_0}{2 \cdot v}$ wavelength in dielectric

The guide wavelength in the air-filled section is

$$\lambda_g := \frac{\lambda_0}{\sqrt{1 - \left(\frac{\lambda_0}{2 \cdot a}\right)^2}} \quad \lambda_g = 0.031 \quad \lambda_0 = 0.03$$

The guide wavelength in the dielectric-filled section is

$$\lambda_g := \frac{\lambda_d}{\sqrt{1 - \left(\frac{\lambda_d}{2 \cdot a}\right)^2}} \quad \lambda_g = 0.015 \quad \lambda_d = 0.015$$

The TE mode impedances are, using $Z_0 = 376.7$ ohm $Z_0 := 376.7$

$$Z_{TEair} := \frac{376.7}{\sqrt{1 - \left(\frac{\lambda_0}{2 \cdot a}\right)^2}} \quad Z_{TEair} = 394.863 \quad \text{ohms}$$

$$Z_{TEdiel} := \frac{376.7}{2 \cdot \sqrt{1 - \left(\frac{\lambda_d}{2 \cdot a}\right)^2}} \quad Z_{TEdiel} = 190.502$$

alternative expressions

$$Z_{TEair} := \frac{Z_0}{\sqrt{1 - \left(\frac{v_c}{v}\right)^2}} \quad Z_{TEair} = 394.863$$

$$Z_{TEdiel} := \frac{Z_0}{2 \cdot \sqrt{1 - \left(\frac{v_{dc}}{v}\right)^2}} \quad Z_{TEdiel} = 190.502$$

Use the transformed impedance formula, write

$$Z_L := Z_{TEair} \quad Z_2 := Z_{TEdiel} \quad Z_1 := Z_{TEair}$$

$$d := 10 \cdot 10^{-3} \quad \text{thickness of slab}$$

$$\beta l := 2 \cdot \frac{\pi}{\lambda_g} \cdot d \quad \text{phase factor to use in transformed impedance equation see for example Eq. 5.7 (13) in RWD}$$

$$Z_i := Z_2 \cdot \frac{(Z_L \cdot \cos(\beta l) + i \cdot Z_2 \cdot \sin(\beta l))}{Z_2 \cdot \cos(\beta l) + i \cdot Z_L \cdot \sin(\beta l)} \quad \text{transformed impedance formula}$$

$$Z_i = 118.156 - 85.223i$$

$$\rho := \frac{(Z_i - Z_1)}{Z_i + Z_1} \quad \text{reflection coefficient}$$

The fraction of energy transmitted is

$$T := 1 - (|\rho|)^2$$

$$T = 0.69$$