

**ENEE 496 Spring 2004**

**Problem Set 2. Due March 4, 2004**

- (1) Davis Problem 2.1
- (2) Davis Problem 2.3
- (3) Davis Problem 2.4
- (4) Davis Problem 2.5
- (5) Davis Problem 2.6
- (6) Davis Problem 2.7
- (7) Davis Problem 2.8
- (8) Davis problem 2.9

(2.1)

$$\gamma_0(\nu_0) = 0.6 \text{ m}^{-1} \quad l = 3 \text{ m}$$

$$I_s(\nu_0) = 3 \text{ W m}^{-2}$$

$$I_0 = 2.5 \text{ W}$$

(a) Input at line center, no saturation included

$$I = I_0 e^{\gamma_0 l} = 2.5 e^{1.8} = \underline{15.124 \text{ W m}^{-2}}$$

(b) Input  $\approx$  1 FWHM from line center

$$\gamma(\nu) = \frac{\gamma_0(\nu_0)}{1 + \left[ \frac{2(\nu - \nu_0)}{\Delta\nu} \right]^2} = \frac{\gamma_0(\nu_0)}{5}$$

$$\gamma(\nu) = 0.12 \text{ m}^{-1}$$
$$I = I_0 e^{0.36} = 2.5 e^{0.36} = \underline{3.5833 \text{ W m}^{-2}}$$

(c)  $I = I_0 e^{\gamma_0(\nu_0) l - (I - I_0)/I_s}$  (A)

$I$  lies somewhere between 2.5 & 15.124 W m<sup>-2</sup>

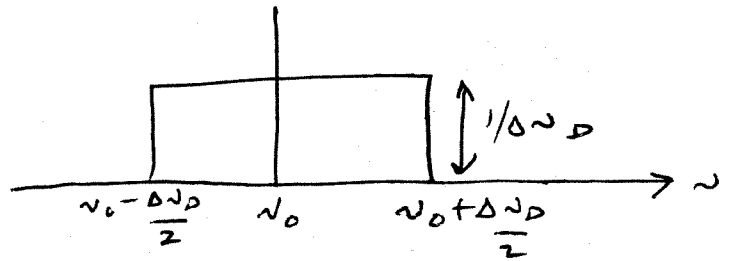
Mathcad gives  $I = \underline{5.522 \text{ W m}^{-2}}$

(d) 1 FWHM from line center  $\gamma_0 = 0.12 \text{ m}^{-1}$

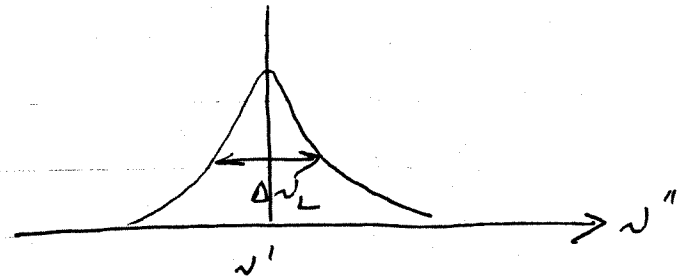
$I_s(\nu) \propto \frac{1}{g(\nu_0, \nu)}$  so  $I_s(\nu) = 15 \text{ W m}^{-2}$

Solve Eq (A) again  $I = \underline{3.379 \text{ W m}^{-2}}$

$$(2.3) \quad g_D(\nu_0, \nu)$$



$$g_L(\nu', \nu'')$$



Overall envelope is

$$g_T(\nu_0, \nu) = \frac{1}{\Delta\nu_D} \int_{\nu_0 - \frac{\Delta\nu_D}{2}}^{\nu_0 + \frac{\Delta\nu_D}{2}} \frac{2}{\pi \Delta\nu_L} \frac{d\nu''}{1 + \left[ \frac{2(\nu - \nu'')}{\Delta\nu_L} \right]^2}$$

Put  $\frac{2(\nu - \nu'')}{\Delta\nu_L} = x$        $d\nu'' = -\frac{\Delta\nu_L}{2} dx$

$$g_T(\nu_0, \nu) = \frac{-1}{\pi \Delta\nu_D} \int_{\frac{2}{\Delta\nu_L}(\nu - \nu_0 - \frac{\Delta\nu_D}{2})}^{\frac{2}{\Delta\nu_L}(\nu - \nu_0 + \frac{\Delta\nu_D}{2})} \frac{dx}{1+x^2}$$

$$= \frac{1}{\pi \Delta\nu_D} \left[ \arctan x \right]_{\frac{2}{\Delta\nu_L}(\nu - \nu_0 - \frac{\Delta\nu_D}{2})}^{\frac{2}{\Delta\nu_L}(\nu - \nu_0 + \frac{\Delta\nu_D}{2})}$$

$$g_T(\nu_0, \nu) = \frac{1}{\pi \Delta\nu_D} \left[ \arctan \frac{2}{\Delta\nu_L} (\nu - \nu_0 + \frac{\Delta\nu_D}{2}) - \arctan \frac{2}{\Delta\nu_L} (\nu - \nu_0 - \frac{\Delta\nu_D}{2}) \right]$$

See following Mathematica plots

$$i = 1, 2, \dots, 1001$$

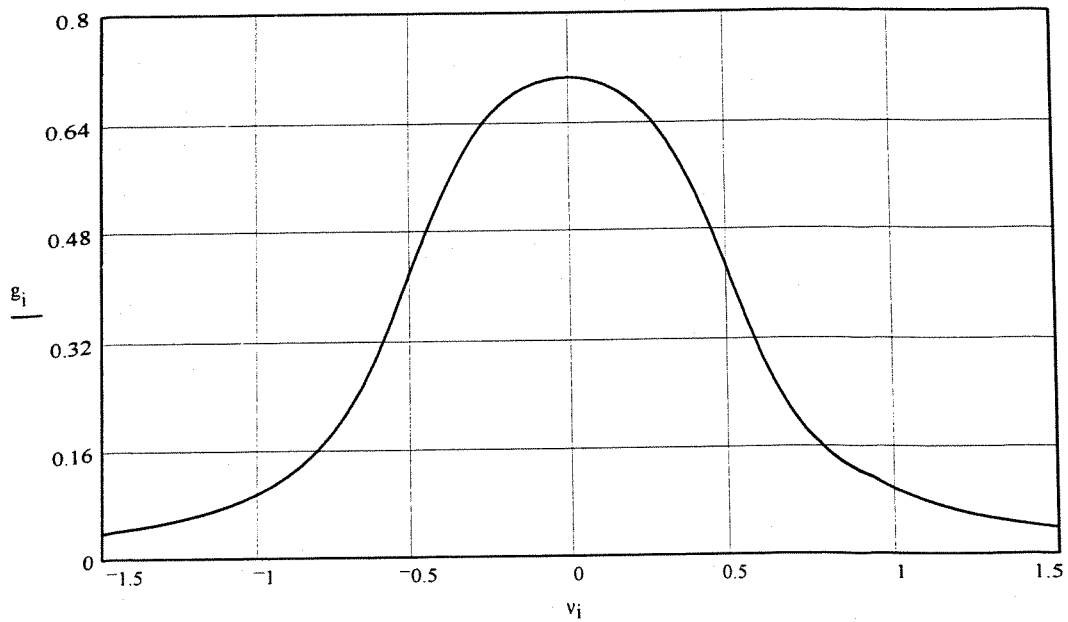
$$\Delta v_D = 1$$

$$\Delta v_L = 0.5$$

$$v_i = -1.5 \cdot \Delta v_D + \frac{i-1}{1000} \cdot 3 \cdot \Delta v_D$$

$$g_i = \frac{1}{\pi \cdot \Delta v_D} \left[ \operatorname{atan} \left[ \frac{2}{\Delta v_L} \cdot \left( \frac{\Delta v_D}{2} + v_i \right) \right] - \operatorname{atan} \left[ \frac{2}{\Delta v_L} \cdot \left( v_i - \frac{\Delta v_D}{2} \right) \right] \right]$$

$$\Delta v_D / \Delta v_L = 2$$



$$\longrightarrow \frac{N - N_0}{\Delta N_0}$$

$$i = 1, 2, \dots, 1001$$

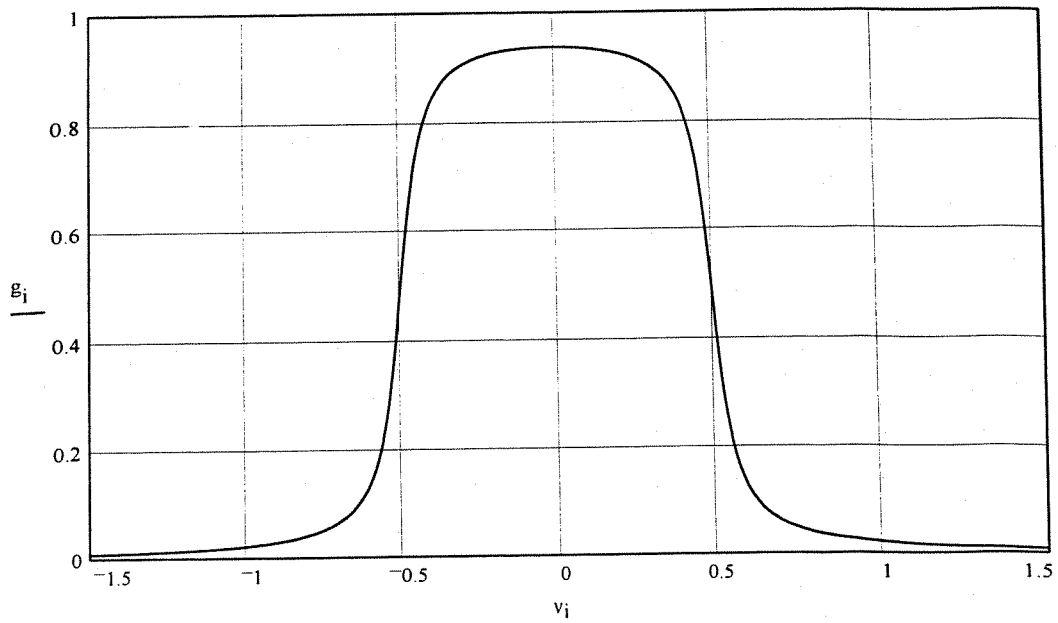
$$\Delta v_D = 1$$

$$\Delta v_L = 0.1$$

$$v_i = -1.5 \cdot \Delta v_D + \frac{i-1}{1000} \cdot 3 \cdot \Delta v_D$$

$$g_i = \frac{1}{\pi \cdot \Delta v_D} \cdot \left[ \operatorname{atan} \left[ \frac{2}{\Delta v_L} \cdot \left( \frac{\Delta v_D}{2} + v_i \right) \right] - \operatorname{atan} \left[ \frac{2}{\Delta v_L} \cdot \left( v_i - \frac{\Delta v_D}{2} \right) \right] \right]$$

$$\Delta v_D / \Delta v_L = 10$$



$$\rightarrow \frac{v - v_0}{\Delta v_D}$$

$$i = 1, 2, \dots, 1001$$

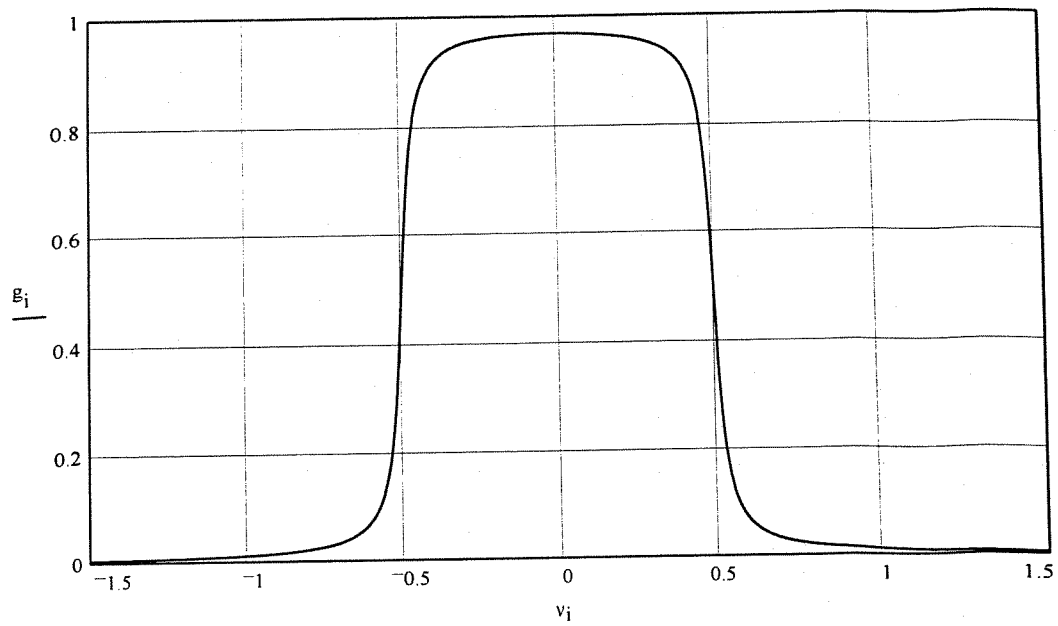
$$\Delta v_D := 1$$

$$\Delta v_L := 0.05$$

$$v_i := -1.5 \cdot \Delta v_D + \frac{i-1}{1000} \cdot 3 \cdot \Delta v_D$$

$$g_i := \frac{1}{\pi \cdot \Delta v_D} \cdot \left[ \operatorname{atan} \left[ \frac{2}{\Delta v_L} \cdot \left( \frac{\Delta v_D}{2} + v_i \right) \right] - \operatorname{atan} \left[ \frac{2}{\Delta v_L} \cdot \left( v_i - \frac{\Delta v_D}{2} \right) \right] \right]$$

$$\Delta v_D / \Delta v_L = 20$$



$$\rightarrow \frac{v - v_0}{\Delta v_D}$$

(2.4) The stimulated emission rate is

$$W_{21}(\nu) = \frac{c^3 A_{21}}{8\pi h\nu^3} g(\nu_0, \nu) \rho(\nu) \quad \text{sec}^{-1} \text{Hz}^{-1}$$

For "white" input radiation

$$W_{21} = \int W_{21}(\nu) d\nu = \frac{c^3 A_{21}}{8\pi h\nu^3} \rho(\nu) \int g(\nu_0, \nu) d\nu$$

$$= \frac{c^3 A_{21}}{8\pi h\nu^3} \rho(\nu)$$

$$= \frac{\lambda^3 A_{21}}{8\pi h} \rho(\nu)$$

For example given  $W_{21} = \frac{(3 \times 10^8)^3 10^8 \times 1}{8\pi \times 6.6 \times 10^{-34} \times 10^{12}}$

$$= \underline{1.6277 \times 10^{23} \text{ s}^{-1}}$$

For monochromatic input

$$W_{21} = \int W_{21}(\nu) d\nu = \frac{c^3 A_{21}}{8\pi h\nu^3} g(\nu_0, \nu) \rho$$

$$\rho = \frac{I}{c} \quad \therefore W_{21} = \frac{c^2 A_{21}}{8\pi h\nu^3} I g(\nu_0, \nu)$$

In the example given  $g(\nu_0, \nu) = \frac{(2/\pi \Delta\nu)}{5}$

$$\therefore W = \frac{c^2 A_{21}}{8\pi h\nu^3} I \left( \frac{2}{5\pi \Delta\nu} \right) = \frac{(3 \times 10^8)^2 \times 10^8 \times 1}{20\pi^2 \times 6.6 \times 10^{-34} \times 10^{12} \times 10^9} = \underline{6.9 \times 10^{11} \text{ s}^{-1}}$$

$$(2.5) \quad \Delta \omega = 10^9 \text{ Hz}$$

$$\gamma_0(\omega_0) = 1 \text{ m}^{-1}$$

$$I_S(\omega_0) = 1 \text{ W m}^{-2}$$

$$l = 0.5 \text{ m}$$

$$I_0 = 2 \text{ W m}^{-2}$$

(a) 500 MHz from line center  $\gamma_c = 0.5 \text{ m}^{-1}$ ,  $I_S = 2 \text{ W m}^{-2}$   
w/o saturation  $I_{\text{out}} = 2 e^{0.25} = 2.568 \text{ W m}^{-2}$

(b) With saturation by Mathcad (see problem 2.1)  
 $I_{\text{out}} = 2.258 \text{ W m}^{-2}$

(c) At line center  $\gamma_0 = 1 \text{ m}^{-1}$ ,  $I_S = 1 \text{ W m}^{-2}$   
with saturation by math cad (see problem 2.1)  
 $I_{\text{out}} = 2.392 \text{ W m}^{-2}$

(d) The 2 signals above and below line center see the same saturation intensity  
Intensity of radiation above line center is  $I_1$   
Intensity of radiation below line center is  $I_2$

$$\frac{1}{I_1} \frac{dI_1}{dz} = \frac{\gamma_0}{1 + (I_1 + I_2) I_S} \quad (i)$$

Write  $I = I_1 + I_2$

$$\frac{1}{I_2} \frac{dI_2}{dz} = \frac{\gamma_0}{1 + (I_1 + I_2) I_S} \quad (ii)$$

guess  $\frac{1}{I} \frac{dI}{dz} = \frac{\gamma_0}{(1 + I/I_S)}$

Substitute in (i)

$$\frac{1}{I_1} \frac{dI_1}{dz} = \frac{\gamma_0}{1 + (I_1^0 + I_2^0) e^{\gamma_0 l - (I_1 + I_2 - I_1^0 - I_2^0)/I_s}} \gamma_0 l - (I_1 + I_2 - I_1^0 - I_2^0)/I_s$$

Substitute in (ii)

$$\frac{1}{I_2} \frac{dI_2}{dz} = \frac{\gamma_0}{1 + (I_1^0 + I_2^0) e^{\gamma_0 l - (I_1 + I_2 - I_1^0 - I_2^0)/I_s}} \gamma_0 l - (I_1 + I_2 - I_1^0 - I_2^0)/I_s$$

where  $I_1^0$  &  $I_2^0$  are the input intensities

This is the exact solution and would need to be solved numerically with  $I_1 = 2 \text{ W m}^{-2}$ ,  $I_2 = 1 \text{ W m}^{-2}$   
 $I_s = 2 \text{ W m}^{-2}$

(2.6) Saturation Intensity is  $I_s(\nu) = \frac{8\pi h\nu^3}{c^2 \phi g(\nu_0, \nu)}$

$$\phi = A_{21} \tau_2 \left[ 1 + (1 - A_{21} \tau_2) \frac{\nu}{\tau_2} \right]$$

$$A_{21} = 10^8 \text{ s}^{-1} \quad \tau_1 = 1 \text{ ns}, \quad \tau_2 = 5 \text{ ns}$$

$$\phi = 10^8 \cdot 5 \times 10^{-9} \left[ 1 + (1 - 10^8 \cdot 5 \times 10^{-9}) \frac{1}{5} \right] = 0.55$$

$$g(\nu_0, \nu) = \frac{2/\pi \Delta\nu}{1 + \left[ \frac{2(\nu - \nu_0)}{\Delta\nu} \right]^2}$$

At 1 FWHM from line center  $g(\nu_0, \nu) = \frac{2}{5\pi \Delta\nu}$

For a naturally broadened system

$$\Delta\nu = \frac{A_1 + A_2}{2\pi} = \frac{10^9 + 0.2 \times 10^9}{2\pi} = 1.91 \times 10^8 \text{ Hz}$$

$$\begin{aligned} \text{So } I_s(\nu) &= \frac{8\pi \times 6.626 \times 10^{-34} \times 2.997 \times 10^8 \times 5\pi \times 1.91 \times 10^8}{10^{-18} \times 0.55 \times 2} \\ &= \underline{1.36 \times 10^4 \text{ W/m}^2} \end{aligned}$$

$$(2.7) \quad \tau = \frac{10^{-8}}{(1+P)}$$

gives a collision broadened linewidth

$$\Delta \nu = \frac{A}{2\pi} = \frac{1}{2\pi\tau} = \frac{1+P}{2\pi \times 10^{-8}}$$

$$\Delta \nu_D = 2\nu_0 \left( \frac{2kT \ln 2}{Mc^2} \right)^{1/2} = \frac{2}{\lambda} \left( \frac{2kT \ln 2}{M} \right)^{1/2}$$

$$M (\text{argon}) = 40 \times 1.67 \times 10^{-27} \text{ kg}$$

$$\text{Take } \lambda = 488 \text{ nm}$$

$$\Delta \nu_D = \frac{2}{488 \times 10^{-9}} \left( \frac{2 \times 1.38 \times 10^{-23} \times 2000 \times \ln 2}{40 \times 1.67 \times 10^{-27}} \right)^{1/2}$$

$$= 3.102 \times 10^9 \text{ Hz}$$

Therefore collisional broadening = Doppler broadening  
when

$$\frac{1+P}{2\pi \times 10^{-8}} = 3.102 \times 10^9 \Rightarrow P = 193.9 \text{ atmosphere}$$

(2.8)  $\chi''(\nu)$  and  $\chi'(\nu)$  vary as in figure (2.16)

The slowest phase velocity will occur where  $\chi'(\nu)$  is a maximum, i.e. at  $\nu = \nu_0 - \Delta\nu/2$

$$\text{Since } \chi'(\nu) = \frac{2(\nu_0 - \nu) \chi''(\nu)}{\Delta\nu}$$

$$\chi'_{\max} = \chi''(\nu_0 - \frac{\Delta\nu}{2})$$

$$\chi''(\nu_0 - \frac{\Delta\nu}{2}) = \frac{1}{2} \chi''(\nu_0)$$

Furthermore  $\chi''(\nu_0) = -\frac{n^2 \gamma(\nu_0)}{k}$

$$\text{so } \chi'_{\max} = \frac{n^2 \gamma(\nu_0)}{2k}$$

Take  $n=1$ ,  $\gamma(\nu_0) = 1 \text{ m}^{-1}$   $k = 2\pi/\lambda_0$

$$\chi'_{\max} = \frac{300 \times 10^{-9}}{4\pi} \Rightarrow \Delta k = \frac{k \chi'_{\max}}{2n^2} = \frac{k}{2} \left( \frac{300 \times 10^{-9}}{4\pi} \right)$$

From Eq. (2.131)  $c' = \frac{c}{1 + \frac{\Delta k}{k}} = c \left( 1 - \frac{\Delta k}{k} \right)$

$$\Delta c = c - c' = \frac{c \Delta k}{k} = \frac{1}{2} \frac{2.998 \times 10^8 \times 300 \times 10^{-9}}{4\pi}$$

$$\Delta c = 3.58 \text{ m/s}$$

The wave slows up by 3.58 m/s

$$(2.9) \quad \Delta \nu = 10^9 \text{ Hz}$$

$$N_2 = 5 \times 10^{16} \text{ m}^{-3}$$

$$N_1 = 5 \times 10^{15} \text{ m}^{-3}$$

$$\lambda_0 = 1 \mu\text{m}$$

$$g_2 = g_1$$

$$A_{21} = 10^8$$

$$\tau_2 = 5 \times 10^{-9}, \tau_1 = 10^{-9}$$

$$(i) \quad \phi = A_{21} \tau_2 \left[ 1 + (1 - A_{21} \tau_2) \frac{g_1}{g_2} \right]$$

$$= 10^8 \times 5 \times 10^{-9} \left[ 1 + (1 - 10^8 \cdot 5 \times 10^{-9}) \frac{1}{5} \right] = 0.55$$

$$I_s(\nu_0) = \frac{8\pi h \nu^3}{c^2 \phi g(\nu_0, \nu)} = \frac{8\pi h \nu^3 \cdot \pi \Delta \nu}{2c^2 \phi}$$

$$= \frac{8\pi \times 6.626 \times 10^{-34} \times 2.997 \times 10^8 \times \pi \times 10^9}{2 \times 10^{-18} \times 0.55}$$

$$= 1.4259 \times 10^7 \text{ W m}^{-2}$$

$$(ii) \quad \chi(\nu) = \frac{(N_2 - N_1) c^2 A_{21}}{8\pi \nu^2} g(\nu_0, \nu)$$

$$= \frac{4.5 \times 10^{16} \times 10^{-12} \times 10^8}{8\pi} g(\nu_0, \nu)$$

$$= 1.79109 (\nu_0, \nu) \text{ m}^{-1}$$

$$\chi'' = \frac{-n^2 \chi}{k} \quad \text{Take } n=1$$

$$\chi'' = - \frac{1.79109 (\nu_0, \nu) \lambda_0}{2\pi} = \frac{1.79 \times 10^5 g(\nu_0, \nu)}{2\pi}$$

$$\chi' = \frac{2(\nu_0 - \nu)}{\Delta\nu} \chi''$$

(iii) At 1 FWHM from line centre

$$g(\nu_0 - \nu) = \frac{2}{5\pi\Delta\nu}$$

Therefore  $\chi'' = \frac{1.79 \times 10^5}{2\pi} \cdot \frac{2}{5\pi \cdot 10^9} = 3.63 \times 10^{-6}$

Therefore  $\chi' = 2\chi'' = 7.255 \times 10^{-6}$

$$\Delta k = \frac{2\pi}{\lambda} \frac{\chi'}{2} = \frac{\pi \times 7.255 \times 10^{-6}}{10^{-6}} = 22.8 \text{ m}^{-1}$$

New phase velocity =  $\frac{\omega}{(k + \Delta k)} = V_p = \frac{\omega}{k(1 + \frac{\Delta k}{k})} = \frac{\omega}{k} \left(1 - \frac{\Delta k}{k}\right)$

Therefore  $\Delta(\text{phase velocity}) \approx -\frac{\omega}{k} \cdot \frac{\Delta k}{k} = -c \cdot \frac{\Delta k}{k}$

$$= -c \cdot \frac{22.8 \cdot 10^{-6}}{2\pi}$$

$$= \underline{4.456 \cdot 10^{-7} c}$$

(2.9) continued

### APPROXIMATE SOLUTION

(iv) If  $\tau_1 = 1 \mu s$  and  $\tau_2 = 5 ns$  the lower level will fill up by transitions from the upper and the population inversion will be transient.

Neglecting stimulated emission  $\frac{dN_2}{dt} = R_2 - \frac{N_2}{\tau_2}$

$$\frac{dN_2}{dt} + \frac{N_2}{\tau_2} = R_2 \longrightarrow N_2 e^{t/\tau_2} = \int R_2 e^{t/\tau_2} dt = R_2 \tau_2 e^{t/\tau_2} + \text{constant}$$

$N_2 = 0$  at  $t = 0$ . Therefore  $N_2 = R_2 \tau_2 (1 - e^{-t/\tau_2})$   
For small  $t$   $N_2 = R_2 t$

$$\frac{dN_1}{dt} = N_2 A_{21} - \frac{N_1}{\tau_1}$$

For small  $t$   $\frac{dN_1}{dt} = N_2 A_{21} = R_2 A_{21} t$

Therefore for small  $t$   $N_1 = \frac{1}{2} R_2 A_{21} t^2$

$$N_2 - N_1 = R_2 t - \frac{1}{2} R_2 A_{21} t^2 = R_2 t \left[ 1 - \frac{1}{2} A_{21} t \right]$$

inversion goes to zero when  $t = \frac{2}{A_{21}} = 20 ns$ .

EXACT SOLUTION

(iv)  $R_2 \rightarrow$   $\text{-----} N_2$   
 $\text{-----} N_1$

Assume that at time  $t=0$ ,  $N_2 = N_1 = 0$

$$\frac{dN_2}{dt} = R_2 - \frac{N_2}{\tau_2} \Rightarrow \frac{dN_2}{dt} + \frac{N_2}{\tau_2} = R_2$$

Multiply each term by  $e^{t/\tau_2}$

$$\frac{dN_2}{dt} e^{t/\tau_2} + \frac{N_2}{\tau_2} e^{t/\tau_2} = R_2 e^{t/\tau_2}$$

Both sides can now be integrated

$$N_2 e^{t/\tau_2} = R_2 \tau_2 e^{t/\tau_2} + \text{constant}$$

From  $N_2 = 0$  at  $t=0 \Rightarrow \text{constant} = -R_2 \tau_2$

Therefore  $N_2 = R_2 \tau_2 (1 - e^{-t/\tau_2})$

$$\frac{dN_1}{dt} = N_2 A_{21} - \frac{N_1}{\tau_1} \Rightarrow \frac{dN_1}{dt} + \frac{N_1}{\tau_1} = R_2 A_{21} \tau_2 (1 - e^{-t/\tau_2})$$

gives  $N_1 e^{t/\tau_1} = \int R_2 A_{21} \tau_2 e^{t/\tau_1} (1 - e^{-t/\tau_2}) dt$   
 $= R_2 A_{21} \tau_2 \tau_1 e^{t/\tau_1} - \frac{R_2 A_{21} \tau_2 e^{(\frac{1}{\tau_1} - \frac{1}{\tau_2})t}}{(\frac{1}{\tau_1} - \frac{1}{\tau_2})} + \text{const.}$

$$N_1 = R_2 A_{21} \tau_2 \tau_1 - \frac{R_2 A_{21} \tau_2 e^{-t/\tau_2}}{(\frac{1}{\tau_1} - \frac{1}{\tau_2})} + \text{const.} \cdot e^{-t/\tau_1}$$

From  $N_1 = 0$  at  $t=0$   $\text{const.} = \frac{R_2 A_{21} \tau_2 - R_2 A_{21} \tau_2 \tau_1}{(\frac{1}{\tau_1} - \frac{1}{\tau_2})}$

Therefore

$$N_1 = R_2 A_{21} \tau_2 \tau_1 (1 - e^{-t/\tau_1}) + \frac{R_2 A_{21} \tau_2}{\left(\frac{1}{\tau_1} - \frac{1}{\tau_2}\right)} \begin{pmatrix} e^{-t/\tau_1} & -e^{-t/\tau_2} \end{pmatrix}$$

The population inversion is  $N_2 - N_1$

$$N_2 - N_1 = R_2 \tau_2 (1 - e^{-t/\tau_2}) - R_2 A_{21} \tau_2 \tau_1 (1 - e^{-t/\tau_1}) - \frac{R_2 A_{21} \tau_2}{\left(\frac{1}{\tau_1} - \frac{1}{\tau_2}\right)} \begin{pmatrix} e^{-t/\tau_1} & -e^{-t/\tau_2} \end{pmatrix}$$

If the inversion is positive then the system will oscillate with appropriate feedback. However, for longer times, since  $\tau_1 > \tau_2$  the inversion will disappear - this is a so-called "SELF-TERMINATING LASER"

For short times

$$N_2 - N_1 = R_2 t - R_2 A_{21} \tau_2 t - \frac{R_2 A_{21} \tau_2}{\left(\frac{1}{\tau_1} - \frac{1}{\tau_2}\right)} \begin{pmatrix} t & -t \end{pmatrix}$$

$$= R_2 t, \text{ which is } > 0$$

For longer times, such that  $e^{-t/\tau_1} \rightarrow 0$

$$N_2 - N_1 = R_2 \tau_2 (1 - e^{-t/\tau_2}) + \frac{R_2 A_{21} \tau_2}{\left(\frac{1}{\tau_1} - \frac{1}{\tau_2}\right)} e^{-t/\tau_2}$$

At very long times

$$N_2 - N_1 = R_2 \tau_2 - R_2 A_{21} \tau_2 \tau_1 - \frac{R_2 A_{21} \tau_2}{\frac{1}{\tau_1} - \frac{1}{\tau_2}}$$

As shown on the accompanying  
Mothcad plot the intrusion disappears  
in the case at fa 1945

(2.9) (iv)

$$R2 = 10^{20}$$

$$\tau2 = 5 \cdot 10^{-9}$$

$$\tau1 = 10^{-6}$$

$$A21 = 10^8$$

$$i = 1, 2, \dots, 1000$$

$$t_i = (2 \cdot i) \cdot \frac{10^{-8}}{999}$$

$$N_i = R2 \cdot \tau2 \cdot \left(1 - e^{-\frac{t_i}{\tau2}}\right) - R2 \cdot A21 \cdot \tau1 \cdot \tau2 \cdot \left(1 - e^{-\frac{t_i}{\tau1}}\right) - R2 \cdot A21 \cdot \tau2 \cdot \frac{e^{-\frac{t_i}{\tau1}} - e^{-\frac{t_i}{\tau2}}}{\left(\frac{1}{\tau1} - \frac{1}{\tau2}\right)}$$

INVERSION VERSUS TIME

